

In-field ambient fine particle monitoring of an outdoor wood boiler: public health concerns

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ABSTRACT

Outdoor wood boilers (OWBs) are detached wood-fired units that heat water used for domestic consumption and heating. The increasing use of OWBs has prompted regulatory concern because of escalating public complaints. Few field studies of OWB ambient emissions have been conducted, limiting efforts to assess this air quality problem. A screening level evaluation was conducted to characterize ambient fine particle ($PM_{2.5}$) levels nearby an OWB device and to overview operating and design factors that could influence $PM_{2.5}$ levels. High hourly ($186 \mu\text{g}/\text{m}^3$ 4.3 hr mean) and peak continuous $PM_{2.5}$ concentrations were found within 50-150 ft of an OWB relative to background levels throughout the course of nearly routine operating conditions. Values were highest during air intake within 1 hr of fuel loading compared to air-starved 22-24 hrs after loading. OWB features that could affect $PM_{2.5}$ levels include exemption from federal wood stove standards, poor combustion design, large firebox capacity, trash burning use, low stack height, and four-season utility. In view of cardiac and respiratory health risks associated with transient exposure to ambient $PM_{2.5}$ at levels well below those reported here, this pilot study contributes to the risk assessment field by identifying an emerging problem of potential public health significance.

Indexing terms: air pollution, $PM_{2.5}$, public health, outdoor wood boiler, residential wood combustion, wood smoke exposure

INTRODUCTION

The use of wood as an alternative to conventional domestic heating fuels is popular in the U.S. and other countries with cold climates, especially during years when fossil fuel availability is uncertain and costs increase relative to renewable fuels (Larson and Koenig 1994; Lipfert and Dungan 1983; Molnár *et al.* 2005; Sexton *et al.* 1984). In recent years, outdoor wood boiler (OWB) sales have occurred in nearly every state in the U.S. Their manufacture and use is increasing, especially in the Midwest, Northeast, and Mid-Atlantic regions. Sales in New York State have tripled since 1999, with over 7,000 OWBs sold from 1999 to 2004. During this time period an estimated 77,500 units have been sold nationwide (Schreiber *et al.* 2005). OWBs are freestanding devices comprised of a firebox and water reservoir, and are detached from living spaces. They have simple fuel requirements and are designed to provide long burns with minimal tending in oxygen-starved combustion conditions. Heated water is piped to a nearby residence for year-round domestic consumption, as well as to heat living spaces (see Figure 1).

Wood burning in populated areas has long raised public health concerns because of health risks associated with inhalation of wood combustion emissions. Wood smoke is comprised of numerous constituents, including volatile organic compounds (VOC), gas-phase and particle-phase polycyclic aromatic hydrocarbons (PAH), carbon monoxide, and fine particles 2.5 microns or less in diameter (PM_{2.5}) (Kozinski and Saade 1998; Oanh *et al.* 1999; USEPA 1993). Numerous studies have found that exposure to the concentrations and durations of wood smoke associated with residential wood burning is likely to cause a variety of adverse respiratory effects. These include increases in respiratory symptoms, decreases in lung function, visits to emergency departments, and hospitalization (Koenig *et al.* 1993; Naeher *et al.* 2005; Pierson *et al.* 1989; Zelikoff *et al.* 2002).

Exposure to fine particles may play a large role in observed health outcomes connected to wood smoke. Because of its physical structure, PM_{2.5} can bypass conductive airways and deliver exogenous materials, such as reactive organic chemicals that adsorb onto the particle core, into the deep lung. Particulate matter from residential wood combustion is largely comprised of submicron particles with average mass diameters generally between 0.1 and 0.6 µm (Hueglin *et al.* 1997; Kleeman *et al.* 1999; Purvis and McCrillis 2000; Rau 1989). Studies of PM in urban areas have found associations of short- (daily) and long-term (annual and multiyear) exposure to airborne PM as well as PM_{2.5} with cardiopulmonary health outcomes. These effects include increased symptoms, hospital admissions and emergency room visits, and premature death (Pope *et al.* 2004). A review of daily 24-hr exposure to PM in study areas where residential wood combustion was considered a major ambient PM source concluded there was no reason to think that adverse health impacts of acute wood smoke exposure would be less than those found in areas dominated by other PM sources (Boman *et al.* 2003).

Very short-term transient (minutes to hours) PM_{2.5} elevations are also of concern. Studies have found associations between 1-12 hr exposures to PM_{2.5} or PM₁₀ and acute cardiovascular and respiratory events, including myocardial infarction in older adults and asthma symptoms in children (Adamkiewicz *et al.* 2004; Delfino *et al.* 1998, 2002; Gold *et al.* 2000; Henneberger *et al.* 2005; Mar *et al.* 2005; Morgan *et al.* 1998; Peters *et al.* 2001). In addition, population subgroups identified as susceptible to health effects as a result of acute and chronic PM_{2.5} exposure comprise a large percentage of the general population (upwards of 50%), including children, asthmatics, persons with respiratory or heart disease, diabetics, and the elderly (Johnson and Graham 2005).

Despite the known health risks of PM exposure, residential wood combustion is one of the largest sources of PM_{2.5} emissions to the atmosphere in North America (Fine *et al.* 2002). Studies in urban and rural locales and regions have found wintertime residential wood combustion emissions can contribute significantly to and even consist of the majority of ambient concentrations of PM_{2.5} as well as VOCs (Fine *et al.* 2001; Maykut *et al.* 2003; McDonald *et al.* 2000; Polissar *et al.* 2001; Schauer and Cass 2000). Woodstove emissions can dominate ambient air levels in areas subject to air stagnation, located in valleys, or which have a high percentage of wood burning households (McGowan *et al.* 2002; Sexton *et al.* 1984). During an inversion, even a small number of woodstoves can affect a large fraction of a community by polluting the local airshed with combustion emissions.

Particles in wood smoke emitted from chimneys have been found to be a major source of indoor particles and accordingly a source of exposure to residents, even in homes without woodstoves (Anuszewski *et al.* 1998; Larson *et al.* 2004). This is attributed to the ability of outdoor PM_{2.5} to infiltrate residential structures, remain suspended indoors, and contribute significantly to indoor particle levels as a result of normal air exchange. Studies have found that indoor fine particles are comprised from about an average of 20% to 80% of outdoor fine particles, depending on climate, building characteristics, and other factors (Abt *et al.* 2000; Allen *et al.* 2003; Dockery and Spengler 1981; Meng *et al.* 2005). Because most people spend up to 90% of their time indoors, individuals receive a substantial fraction of their exposure to outdoor-generated particles while they are indoors. Recent studies suggest that the ambient-generated component of PM_{2.5} exposure is associated with measures of adverse health outcomes, more so than indoor-generated PM_{2.5} components (Ebelt *et al.* 2005; Koenig *et al.* 2005).

Although residential wood burning emissions can comprise a substantial fraction of indoor PM_{2.5}, the majority of U.S. wood stoves in current use were manufactured without consideration of particulate emissions control. Public health concerns prompted the U.S. Environmental Protection Agency (EPA) to promulgate regulations requiring residential wood heaters manufactured on or after July 1, 1990, or sold at retail on or after July 1, 1992, to produce clean-burning stoves with efficient combustion designs or pollution control devices to reduce PM emissions. Indoor woodstoves manufactured prior to 1990 contained inadequate combustion design or lacked emissions controls. EPA has estimated that certified (post-1990) woodstoves generate from 70-90% less PM than pre-1990 non-certified or conventional models (USEPA 1988, 1990, 1998a). Since 1992, however, EPA has certified about 20-30% of all woodstoves and fireplace inserts for low PM emissions, suggesting a 2% annual change-out rate of pre-EPA-certified woodstoves (Broderick and Houck 2005). This indicates that upwards of 80% of the current woodstove fleet was manufactured without efficient combustion designs or pollution control devices required since 1990.

During the past two decades, woodstove and fireplace insert ownership in the U.S. has been static, numbering about 14-17 million appliances. About 12 million of these appliances are used for either primary (~20%) or supplemental (~80%) heating, suggesting the capacity for substantial increases in wood burning should more owners move to primary use (Broderick and Houck 2005). New England has the highest per capita woodstove ownership in the U.S., and the Northeast Census Region (New England, New Jersey, New York, and Pennsylvania) consumes over twice the number total cords of wood in woodstoves per year than the Midwest, South, or West (Houck *et al.* 2001).

The increasing use of outdoor wood boilers could hinder ongoing regulatory efforts to reduce residential wood combustion emissions. EPA's current wood stove PM emissions standards exclude OWBs, which can be manufactured without efficient combustion design or emissions control systems. To date, limited emissions testing suggests that OWB PM emissions are higher than pre-certified indoor woodstoves manufactured before 1990; emissions are also higher than EPA-certified woodstoves manufactured after 1990 (USEPA 1998a; Schreiber *et al.* 2005). OWB use has led to a growing number of air quality complaints by residential neighbors, prompting local government and state regulatory attention (e.g., Colburn 2004; CTDEP 2004; Spitzer 2005; WIDPH 2005). Adequate regulatory response to this air quality problem requires a better understanding of OWB emissions, especially in areas adjacent to these devices. This study conducted a screening level evaluation to characterize ambient PM_{2.5} emissions nearby an OWB device. The study also assessed operating and design factors unique to OWBs that could influence PM_{2.5} levels.

METHODS

Exploratory field sampling in March 2005 was conducted in central New York State on the residential property of an OWB owner. The OWB unit was a Hardy Manufacturing Company, Inc. H5-1-07 "Economy" model manufactured in November 1998 (Hardy Manufacturing Company 2005). The current owner purchased the unit in 2003. Stack height from the ground was about 9 ft, fire chamber capacity was 22.6 ft³, maximum capacity output was 180,000 btu/hr, and water capacity was 130 gallons. The OWB water thermostat was set at 91°C. An electronic combustion blower, or damper control, governed OWB air intake. The owner used the OWB to heat two household radiant zones and to provide domestic hot water.

Fuel usage during fieldwork monitoring was a mix of green oak logged November 1, 2004 (split December 2004) and maple/cherry/other hardwood seasoned about one year. All fuel wood was stored “dry” under cover in an open-ended metal carport, with minimal weathering occurring along the wood pile periphery.

Screening level monitoring nearby the OWB attempted to characterize PM_{2.5} levels with respect to time from last fuel loading and to damper open (oxygen rich) and damper closed (oxygen starved) boiler operating modes. Highly time-resolved PM_{2.5} monitoring was conducted in order to capture the variability of concentration levels influenced by these two dynamic parameters. This required the use of a continuous light scattering device because of its suitability as an indicator of short-term variations in PM_{2.5} mass concentrations and particle size (Chow *et al.* 2002). The Thermo MIE DataRAM 4 (Model DR 4000) was selected for its ability to provide real time ambient PM_{2.5} mass concentration measurements and for its favorable performance under rigorous environmental conditions (Thermo Electron Corporation 2005).

The DataRAM 4 (DR) is a portable two-wavelength (660 and 880 nm) nephelometric monitor that employs light scattering with active air sampling (1-3 L/min). The magnitude of the detected light scatter at either of the two wavelengths is directly proportional to the amount of particles passing through the device’s sensing region. Based on the ratio of the responses at the two different wavelength signals, the volume median particle aerodynamic diameter is determined (0.04 to 4.0 μm range), which is used to compute the mass concentration (0.1 μg/m³ to 400,000 μg/m³ range). The instrument can measure PM_{2.5} in combination with an inertial coarse-particle precollector (e.g., impactor) that removes the particle population typically larger than an aerodynamic diameter of 2.5 μm. The test dust used for the factory calibration of the instrument is SAE Fine (ISO Fine) with a mass median aerodynamic particle diameter of 2 to 3

μm , a geometric standard deviation of lognormal size distribution of 2.5, a bulk density of 2.60 to 2.65 g/cm^3 , and a refractive index: 1.54. Regarding the possible influence of relative humidity on light scattering measurements, the DR autocorrects for airborne particles likely to grow by accretion of water. This typically occurs at ambient relative humidity above 65 to 70% and is generally negligible up to about 50%. The instrument can function in an operating environment of -10 to 50 °C and 10 to 95% relative humidity (Thermo Electron Corporation 2005).

In-field monitoring near the Hardy OWB was conducted on two separate late afternoon/early evening periods for a total elapsed time of 4.3 hrs using a time average concentration log period of 15 seconds. Background/upwind $\text{PM}_{2.5}$ data were collected before commencing sampling on each day. The DR had been recently factory calibrated and was zeroed just prior to sampling on each field day. On-site AC power was used to run the instrument continuously throughout sampling; the DR was acclimated to outdoor temperatures before operating. An assembly in-line impactor head $\text{PM}_{2.5}$ cut point and omnidirectional sampling inlet precipitation shield were used to sample particles representatively. The DR's internal temperature and relative humidity sensors used to record these environmental variables have measurement ranges of -15 to 60 °C (accuracy 0.5 °C) and 0 to 100% (accuracy 2%), respectively. Precipitation, wind speed, and wind direction (of the OWB plume) were observed.

Fine particle measurements were recorded during nearly routine OWB operating conditions relating to fuel loading and oxygen demand parameters on two days. Sampling was conducted within 22-24 hrs after fuel loading (day 1 and day 2) and from 0-1 hr after fuel loading (day 2). The OWB unit controlled damper open/closed modes, which household demand regulated at a pre-selected water thermostat temperature (91°C). Manipulation of the oxygen supply parameter was limited to sampling in the late afternoon when the unit was transitioning

from low to moderate/high usage and to occasional manual damper override by means of cutting the damper's electricity source.

The influence of fine particle sources during sampling in the vicinity of OWB unit was minimal. The unit was located in a rural area at a residential site about 200 ft west of a county road with periodic traffic traveling at relatively constant speeds in excess of 45 mph. The unit was about 60 feet from the owner's residence. A northwesterly transect away from the OWB, house, and road was selected to maximize sampling time along an unobstructed line and minimize the contribution of local $PM_{2.5}$ sources. The transect avoided direct obstructions adjacent to the OWB stack, including an open-ended carport used for wood storage perpendicular to the unit with a peak height of 10 ft. The line followed the contour of a field rising slightly upslope of the OWB toward woods, about 5 vertical ft higher than the base of the OWB at the 150 ft horizontal distance. The sampling inlet attached to the DR was about 3 ft above ground in an upright position. Sampling distances along the transect were pre-measured at 50-, 100-, 130-, and 150-ft intervals to simulate near-site residential locations. The nearest actual neighbors were several hundred feet north and south of the OWB. No neighbors were located west or east of the unit.

RESULTS

Screening level continuous ambient $PM_{2.5}$ monitoring nearby the Hardy OWB attempted to characterize particulate levels relating to time since last fuel loading and to damper open (oxygen rich) and damper closed (oxygen starved) operating mode. Table 1 summarizes sample size results for these parameters. A total of 1,032 15-second sampling intervals (258 minutes or 4.3 hrs) were recorded during two late afternoon/early evening periods overlapping a customary

diurnal period of domestic hot water demand (day 1, 16:00-16:50; day 2, 14:55-18:30). Seventy-six percent of the PM_{2.5} monitoring data (197 minutes) were collected within 22-24 hrs after the OWB appliance had been last loaded with one wheelbarrow of wood previous to day 1 and day 2 sampling. The remaining 24% of the data (61 minutes) were collected within 0-1 hr after the appliance had been loaded with one-half wheelbarrow load of wood on day 2 sampling. Sixty percent of the sampling intervals (154 minutes) occurred when the OWB was drawing air (damper open) and 40% (104 minutes) occurred when the OWB was not drawing air (damper closed). Thirty-two percent of the samples were recorded at 150 feet; 20%, 36%, and 12% were recorded at 130, 100, and 50 feet, respectively. During monitoring, temperature ranged from 1.7 to 15.1 °C and relative humidity ranged from 28 to 55%. Wind speed and direction with respect to the OWB plume were visually observed to be calm/variable with periodic light southerly, easterly, and northerly winds. Light snow and periods of no precipitation were intermittent.

Table 2 presents 15-second average PM_{2.5} percentile and mean values within 50-150 feet of the OWB during sampling periods 22-24 hrs and 0-1 hr since last wood loading. Table 3 presents PM_{2.5} values aggregated by time since last wood loading at different distances within 50-150 feet from the OWB. Both tables provide data relating to damper open, damper closed, and aggregated damper operating modes.

As shown in Table 2, the PM_{2.5} median for the entire 258-minute sampling period was 58 µg/m³, with a mean value of 186 µg/m³, during which the damper was open about 154 minutes (mean value 235 µg/m³) and closed about 104 minutes (mean value 113 µg/m³). These values were high relative to background levels collected upwind of the OWB during each day's sampling (<20 µg/m³). Damper open/closed sampling intervals were fairly consistent for

purposes of comparison, with 60% of the samples collected while the damper was open and 40% while closed.

Table 2 also provides findings with respect to time since last fuel loading, although the sampling intervals were less consistent. Seventy-six percent of the samples were collected 22-24 hrs after loading and 24% were collected within 1 hr of loading. Mean recorded $PM_{2.5}$ values were high relative to background during both damper open (oxygen rich) and closed modes (oxygen starved) at both 22-24 hrs ($115 \mu\text{g}/\text{m}^3$ aggregated) and 0-1 hr ($416 \mu\text{g}/\text{m}^3$ aggregated) since last fuel loading. The higher levels observed within 0-1 hrs from fuel loading were influenced by differences between damper open values. Damper open concentrations 0-1 hr since last fuel loading were substantially higher than damper open concentrations 22-24 hrs since last loading (838 vs. $118 \mu\text{g}/\text{m}^3$), whereas damper closed concentrations were similar (118 vs. $110 \mu\text{g}/\text{m}^3$). Across both damper modes and times from loading, 95th percentile and maximum values were high relative to background, although maxima 0-1 hr from loading were substantially higher than 22-24 hrs maxima. A peak 15-second value of $8,880 \mu\text{g}/\text{m}^3$ was observed.

Table 3 shows recorded $PM_{2.5}$ data ranges at four sampling distances located between 50-150 feet from the OWB unit. Mean values during damper closed modes were generally similar across distances 100-150 feet, and lowest at 50 feet from the OWB. Damper open mode values tended to increase as the monitor was placed closer to the OWB. All percentile metrics were highest at the 50 feet sampling location when the damper was opened. Within each sampling distance and damper mode category, fine particle maxima were substantially higher relative to mean values. Because sampling intervals at varying distances were not uniform, it is difficult to draw meaningful comparisons across distances and damper modes.

Figures 2 and 3 present two time-series sampling periods selected from the larger dataset. The figures illustrate how dynamic operating conditions and wind direction in relation to plume movement influenced measured concentration levels. As summarized in Table 4, the time series plot in Figure 2 shows 15-second average $PM_{2.5}$ values about 24 hrs after the unit was loaded with one wheelbarrow of wood fuel per day (on two consecutive days). Figure 3 shows $PM_{2.5}$ time-series values recorded during and up to about 1 hr after the unit was loaded with one-half wheelbarrow of wood fuel (about 24 hrs after the unit had previously been loaded with a full wheelbarrow of wood the day before).

In both figures, visual field observations taken during monitoring indicate that as the DR instrument varies from being directly downwind to not directly downwind of the OWB plume, recorded $PM_{2.5}$ concentrations changed. High $PM_{2.5}$ values relative to background were found when the plume was observed blowing over the monitor, with noticeable drops in concentration as the plume was observed moving away from the transect and emissions dispersed, explaining much of the peak and trough appearance of the data. Monitored values upwards of $1,000 \mu\text{g}/\text{m}^3$ occurred at 130 ft from the OWB even though the boiler had been fuel-starved for nearly one day. Within 1 hr of fuel loading, values upwards of $5,000 \mu\text{g}/\text{m}^3$ were recorded at 100 ft, where a peak 15-second average of $6,717 \mu\text{g}/\text{m}^3$ was monitored.

DISCUSSION

This screening level evaluation characterized $PM_{2.5}$ levels nearby an OWB device under different operating conditions. The study found that transient fine particle emissions (1-4 hr averages) were high relative to background levels. Real time concentrations varied according to damper open (oxygen rich) and closed (oxygen starved) modes, time since last fuel loading,

monitor distance from the OWB, and location of monitor with respect to the center of the plume. Overall, the mean $PM_{2.5}$ level during the entire 4.3 hr study period was $186 \mu\text{g}/\text{m}^3$. When the OWB was drawing oxygen (damper open), the mean value recorded was $235 \mu\text{g}/\text{m}^3$ (2.6 hr) versus $113 \mu\text{g}/\text{m}^3$ (1.7 hr) during oxygen starved (damper closed) conditions. Within 0-1 hr after fuel loading, the study $PM_{2.5}$ mean was $416 \mu\text{g}/\text{m}^3$ (1 hr); within 22-24 hr after fuel loading, the mean was $115 \mu\text{g}/\text{m}^3$ (3.3 hr). High 15-second average maxima were observed regardless of damper mode status, fuel loading time, and monitoring distance. Plume movement over and away from the monitor was an important variable affecting fine particle concentration levels.

These findings raise public health concerns because of acute respiratory and cardiac events associated with transient exposures to $PM_{2.5}$ at levels well below those reported in this study. For example, in a semirural area of southern California, Delfino *et al.* found same-day associations between 1-hr and 8-hr maximum PM_{10} levels and children's asthma episodes, noting that most pollutant effects were largely driven by concentrations in the upper quintile. Mean (standard deviation) 1-hr and 8-hr maximum PM_{10} values were $38(15) \mu\text{g}/\text{m}^3$ and $28(12) \mu\text{g}/\text{m}^3$, respectively (Delfino *et al.* 2002). Recently, in Seattle Mar *et al.* reported associations between hourly exposures to $PM_{2.5}$ and the fractional concentration of nitric oxide (a marker of airway inflammation and injury) measured in exhaled breath of children with asthma. One-hour averaged concentrations ranged from $8.3 \mu\text{g}/\text{m}^3$ at 3-hr lag to 15.2 at 8-hr lag (Mar *et al.* 2005).

Regarding transient $PM_{2.5}$ exposure and acute cardiac events, in the greater Boston area Peters *et al.* found that elevated concentrations of $PM_{2.5}$ were associated with a transient risk of acute myocardial infarction (MI) onset in a study population whose mean age was about 62 years. Associations were observed 1 hr and 2 hrs before the onset of symptoms. Even changes from low to moderate ambient concentrations were associated with an increased risk of MI. The

mean (standard deviation) 1-hr level was 12.1(8.9) $\mu\text{g}/\text{m}^3$, with a 95th percentile value of 29.6 $\mu\text{g}/\text{m}^3$ (Peters *et al.* 2001). In the same city, Gold *et al.* reported alterations of autonomic function through decreases of heart rate variability within hours of exposure to $\text{PM}_{2.5}$. Mean 4-hr $\text{PM}_{2.5}$ levels ranged from 3-49 $\mu\text{g}/\text{m}^3$ (Gold *et al.* 2000). Finally, in Sydney Australia Morgan *et al.* found that an increase in current day maximum 1-hr particulate concentration from the 10th to the 90th percentile was associated with an increase of cardiovascular mortality. The study's mean $\text{PM}_{2.5}$ concentration was 21 $\mu\text{g}/\text{m}^3$, with 10th and 90th percentile values of 6.9 and 42.6 $\mu\text{g}/\text{m}^3$ (Morgan *et al.* 1998).

In addition to emitting high transient fine particle levels, outdoor wood boilers have other attributes that make them a unique emissions source and potential public health threat. Unlike traditional wood combustion sources such as indoor woodstoves and fireplaces, OWBs are controlled by an automatic damper that follows the heat load of a residence. This results in intermittent combustion cycles characterized by alternative high-temperature oxygen-rich burns and low-temperature oxygen-starved burns. In general, both burn cycles generate elevated $\text{PM}_{2.5}$ levels. However, during smoldering conditions, increasing $\text{PM}_{2.5}$ mass concentration yields condensable gas and organic condensation nuclei (Barrefors and Petersson 1995; Johansson *et al.* 2003; Lighty *et al.* 2000). Primitive OWB combustion designs do not oxidize these incomplete combustion vapors, leaving them available for the formation of fine particles rich in relatively high molecular weight organic compounds (Hueglin *et al.* 1997; McDonald *et al.* 2000).

The use of OWBs for trash burning heightens the potential public health threat related to these devices. Sizeable firebox capacity and large loading door dimensions characteristic of OWBs facilitate the loading and burning of non-wood materials such as household waste (e.g., paper, plastic, and packaging). The combustion of trash in devices that lack emissions control

systems and in low temperature conditions creates favorable conditions for generating hazardous air pollutants. Using OWBs to burn trash could be analogous to the use of burn barrels and burn piles, which many states and local governments have banned because a variety of pollutants are emitted, including acidic gases, heavy metals, and dioxin. Inhaling these substances may cause health problems including eye and throat irritation, respiratory problems, and an increased risk of cancer. EPA burn barrel test burns found that emission levels of dioxin, VOCs, and PAHs were significantly higher than those of a full-scale municipal solid waste combustor, or incinerator, with control technology (USEPA 1998b).

Finally, in contrast to indoor woodstove stacks that extend through the roof of a home to heights of 20 to 30 ft, OWBs are supplied with short stacks typically 8 to 10 ft high from the ground. The low chimney height of these devices relative to downwind nearby residences creates the opportunity for poor dispersion conditions, including an increased likelihood of worst-case exposure scenarios such as fumigation and impingement. The possible impact on nearby residences is exacerbated because OWBs can be used to supply hot water every day, all year – not just during wintertime.

This screening level OWB field monitoring could have benefited from a more consistent set of sampling periods across distance and time since fuel loading parameters. This was constrained in part because the specific timing of OWB damper open/closed modes was unpredictable and variable, as it was controlled largely by automatic boiler operating demands. While allowing the OWB to operate in nearly routine field conditions enabled sampling to occur across nearly standard fuel load and oxygen demand modes, it limited the ability to conduct uniform sampling periods over the 4.3 hr study time frame.

Lack of wind measurement data also limited the interpretation of $PM_{2.5}$ values across different parameters, including damper open/closed modes, time after fuel loading, and monitoring distance. However, visual observations of plume movement demonstrated the importance influence that plume variability had on recorded fine particle levels. Higher concentrations likely could have been recorded if wind speed and direction had carried the plume over the monitor consistently during the sampling period, or if the study site had been experiencing an inversion. Also, the possibility of recording higher monitored levels is not unlikely because the study monitored an 180,000 btu/hr OWB boiler “economy” model. OWB boiler models range from about 100,000 to >500,000 maximum btu/hr output.

Because the transient $PM_{2.5}$ concentrations measured by the DataRAM 4 nearby an OWB in this study were high relative to background concentration, the application of a large correction factor with gravimetric PM instrumentation (e.g., 50-100%) would not materially change the overall findings. Sioutas *et al.*'s field assessment found good correlation between DataRAM and gravimetric measurements of $PM_{2.5}$ levels in real time (Sioutas *et al.* 2000). The DataRAM-to-gravimetric concentration ratio was 0.93 (± 0.17) and 1.23 (± 0.20) ratios for ambient or concentrated $PM_{2.5}$ levels, respectively. Sampling times varied from 4-7 hrs for 39 characterizations. Ambient and concentrated 4-7 hr averaged $PM_{2.5}$ levels ranged from 6.7 to 114.0 $\mu g/m^3$ and from 180.5 to 340 $\mu g/m^3$, respectively. The researchers also found that PM chemical composition of urban particles did not affect significantly the response of the DataRAM. These results suggest the feasibility of using DataRAM measurements to characterize $PM_{2.5}$ mass ambient levels recorded in this OWB study, whose mean fine particle concentration was 186 $\mu g/m^3$ for a 4.3 hr period.

The U.S. Forest Service currently uses the DataRAM 4 to provide general trends of ambient wildfire smoke $PM_{2.5}$ concentration in the western U.S., where 1-hr and 24-hr running-average gravimetric levels have been recorded as high as 500 and 284 $\mu\text{g}/\text{m}^3$, respectively. However, the agency recommends using a DataRAM correction factor of 0.37 to 0.48 based on tests finding high overestimations compared to gravimetric sampling when sampling biomass combustion aerosol (USDA 2001-2003). The application of these correction factors to study findings would not materially change study results. Even stringent correction factors would result in high 1-4 hr averages relative to background levels. Nonetheless, a more conservative assessment of these data could interpret the $PM_{2.5}$ concentrations as indicators of general trends relating to monitoring distance from the OWB, boiler operating modes, and time after fuel loading.

In view of this exploratory study's findings of high transient $PM_{2.5}$ emissions relative to background, and because of design and operating factors unique to outdoor wood boilers, this research recommends exposure assessment studies to quantify the nature and magnitude of potential exposure to OWB emissions. Exposure could be influenced by where OWBs are situated in relation to residential structures, as well as by the air exchange characteristics of these structures. Exposure could also be influenced by the geography and meteorological conditions of populated areas that contain OWB units.

Future studies could benefit from monitoring during longer time periods that encompass daily modulations in hot water demand, as well as weekly or seasonal variations in use and fuel demand. This would increase understanding of how meteorological variability, including changes in atmospheric stability, wind speed and direction, temperature, and relative humidity could influence emissions levels experienced by receptors. Because the study found a sizeable

difference in fine particle values between 0-1 hr and 22-24 hrs after fuel loading, characterization of this PM_{2.5} gradient would be worthwhile to determine. Additional consideration should be given to monitoring OWB emissions generated from non-ideal fuels should evidence point to the burning of poorly seasoned wood or trash. Ambient and OWB stack emissions testing of air pollutants relevant to environmental exposures and potential public health concerns should be collected under real-world operating conditions.

Although this pilot study was not intended to quantify 24-hr or longer-term average exposures (e.g., a complete heating season), such information would be useful to collect at different OWB sites because of findings of high transient PM_{2.5} concentrations relative to background levels in proximity to an OWB under routine operating conditions. EPA's national ambient air quality PM_{2.5} standards are based on 24-hr (65 µg/m³) and annual means (15 µg/m³) (USEPA 1997). These standards are currently under review for possible revision. The Clean Air Scientific Advisory Committee has recently recommended a 24-hr standard no higher than 35 µg/m³ and an annual standard no higher than 14 µg/m³ (USEPA 2005).

In conclusion, exploratory ambient monitoring 50-150 ft from an OWB unit operating under nearly routine conditions found high continuous PM_{2.5} concentrations relative to background levels during air intake and starvation modes within about 1 hr and 22-24 hrs after fuel loading. OWB design and usage characteristics represent a unique wood burning emissions source because of inefficient and primitive combustion design, exclusion from current EPA wood stove emission standards, large firebox capacity conducive to trash burning, low ground-level stacks favorable to poor emissions dispersion, and four-season utility. Consideration of these factors suggests that the increasing use of OWBs in populated areas presents a potential emerging air quality problem with public health ramifications. The finding of overall mean

hourly PM_{2.5} values and peak values that are considerably higher than mean hourly and maximum hourly levels reported in recent studies showing acute cardiac and pulmonary adverse health outcomes from inhalation of fine particles lends support to this concern. It also raises an important but unresolved question of the potential magnitude and variability of population exposure to ambient wood smoke, especially in geographic areas such as river basins or valleys prone to meteorological stagnation events that trap wood smoke. This screening level monitoring study recommends future research that would collect monitoring and exposure data of sufficient quality to support the evaluation of potential risks.

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Figure 1. Diagram of an outdoor wood boiler.

Figure 2. Real time field measurements of $PM_{2.5}$ in proximity to an outdoor wood boiler (OWB).

The DataRAM (DR) $PM_{2.5}$ monitor recorded 15-sec average values 130 ft from the emissions source during damper open (oxygen rich) mode about 24 hrs after fuel loading.

Figure 3. Real time field measurements of $PM_{2.5}$ in proximity to an outdoor wood boiler (OWB).

The DataRAM (DR) $PM_{2.5}$ monitor recorded 15-sec average values 100 ft from the emissions source during damper open and closed (oxygen rich and starved) modes during and immediately after fuel loading.

Figure 1.

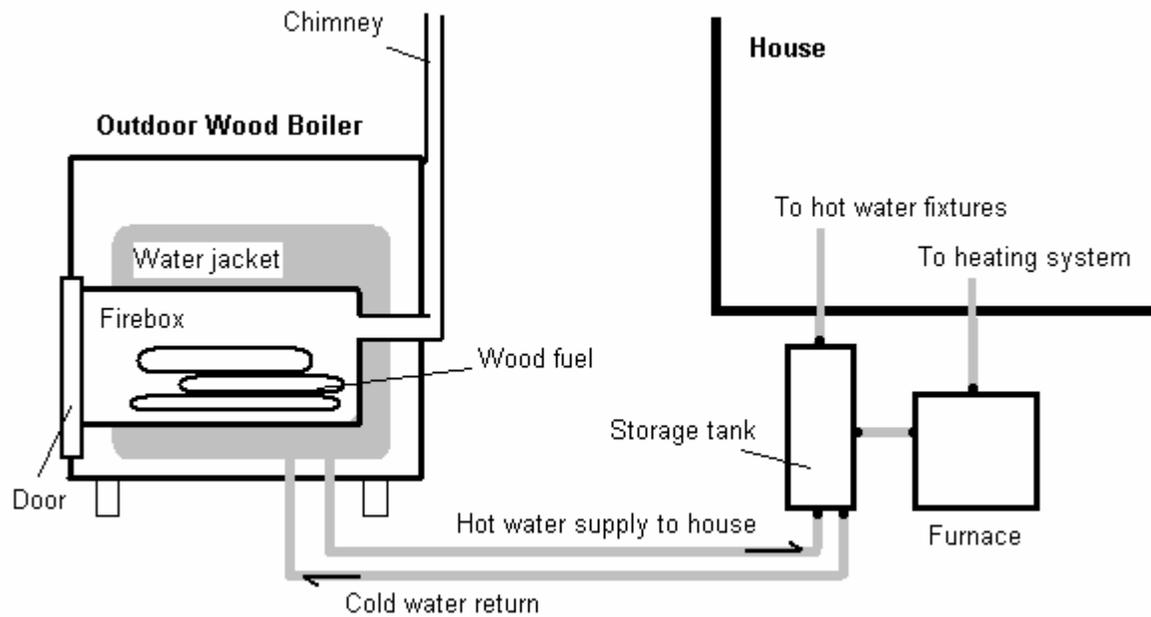


Figure 2.

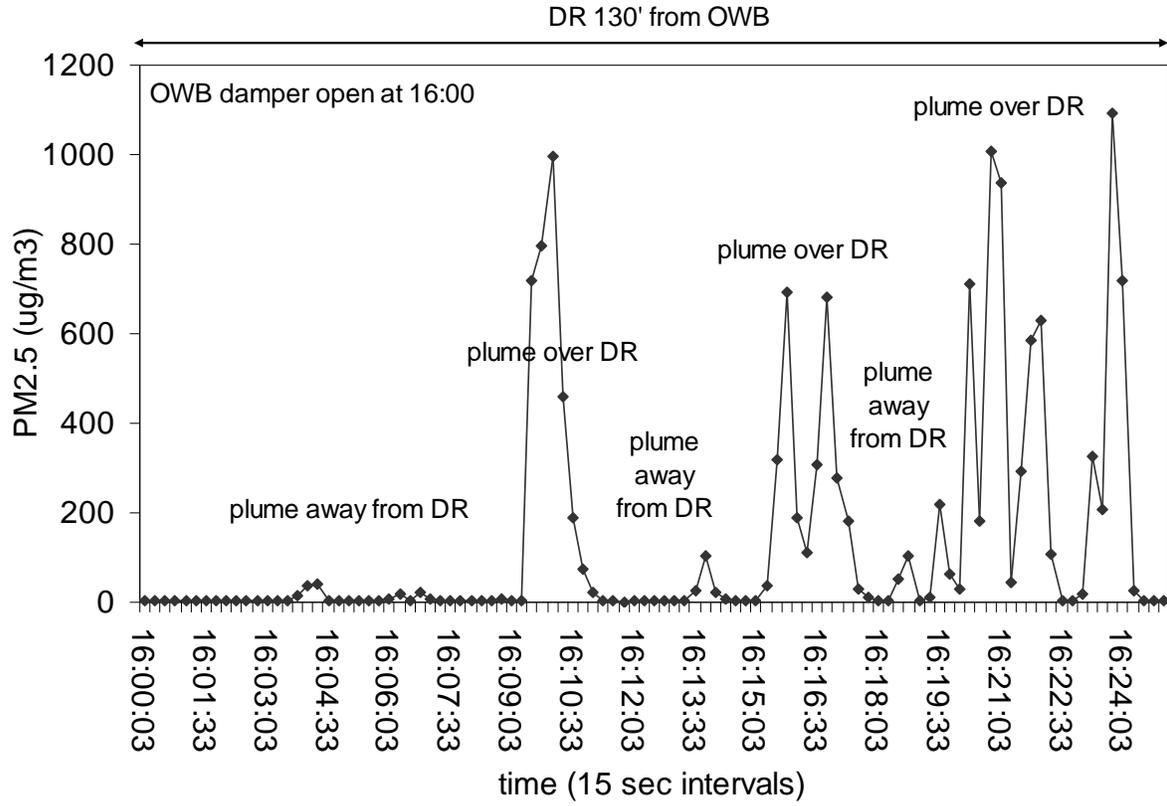


Figure 3.

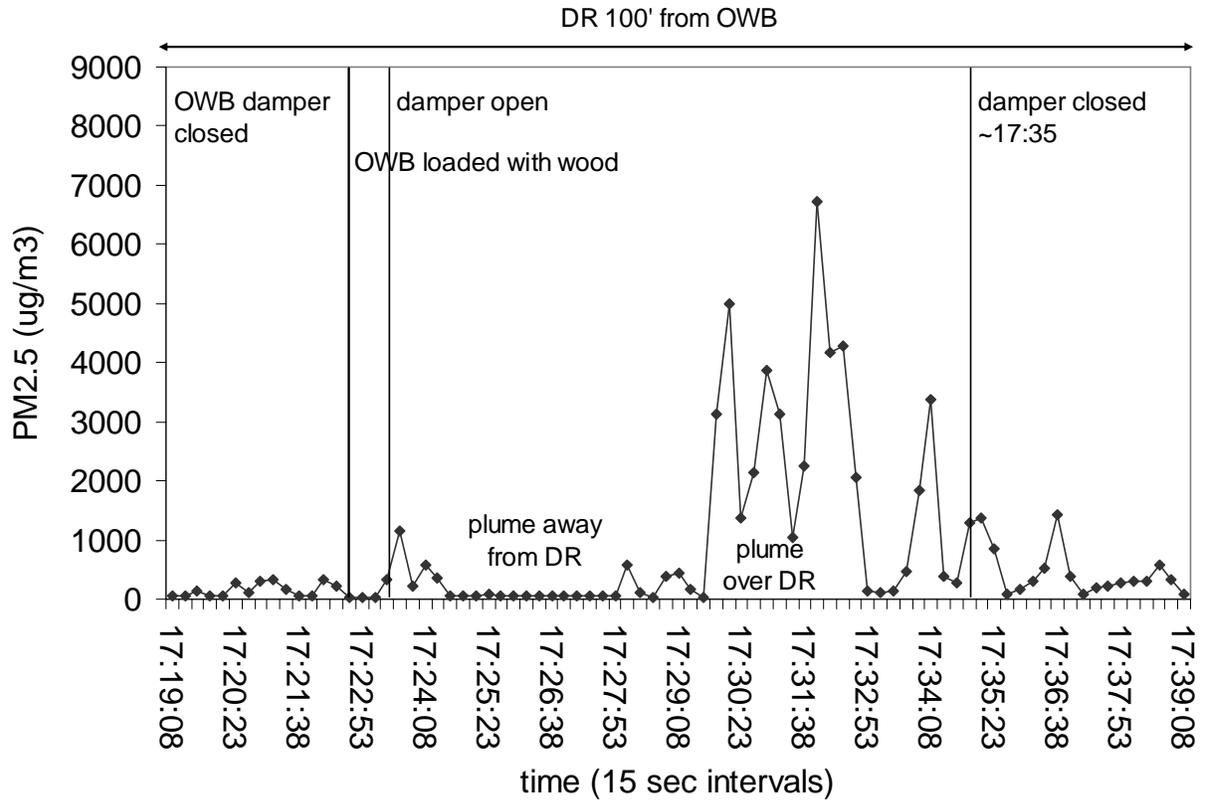


Table 1. Continuous PM_{2.5} sampling effort for time since last fuel loading, aggregate damper mode time, and aggregate monitoring distance time.

Parameter	PM _{2.5} sampling interval (15-sec avg)	Minutes	%
Total sampling effort	1032	258.00	100
Number of hrs since OWB last loaded with wood fuel			
22-24 hrs	788	197.00	76
0-1 hr	244	61.00	24
OWB air intake mode			
damper open, drawing air	617	154.00	60
damper closed, not drawing air	415	104.00	40
Monitoring instrument distance from OWB			
150 ft	336	84.00	32
130 ft	196	49.00	20
100 ft	373	93.25	36
50 ft	127	31.75	12

Table 2. 15-second average PM_{2.5} percentile and mean values 22-24 hrs and 0-1 hr since last fuel loading recorded within 50-150 feet of OWB during damper open and closed modes.

PM _{2.5} 15-sec avg values (µg/m ³)	22-24 hr since last load			0-1 hr since last load			22-24 and 0-1 hr combined		
	damper open	damper closed	open and closed	damper open	damper closed	open and closed	damper open	damper closed	open and closed
minimum	1	2	1	24	26	24	1	2	1
5 th	2	5	3	36	33	35	3	13	3
50 th	63	45	53	177	58	62	70	53	58
mean	118	110	115	838	118	416	235	113	186
95 th	400	412	412	4,170	285	2,241	807	377	665
maximum	1,092	1,071	1,092	8,880	3,328	8,880	8,880	8,880	8,880
sampling intervals (15-sec avg)	516	272	788	101	143	244	617	415	1,032
minutes	129.00	68.00	197.00	25.25	35.75	61.00	154.25	103.75	258.00
%	50	26	76	10	14	24	60	40	100

Table 3. 15-second average PM_{2.5} percentile and mean values recorded within 50, 100, 130, and 150 feet of OWB during damper open and closed modes within 22-24 and 0-1 hr since last wood loading.

PM _{2.5} 15-sec avg values (µg/m ³)	150 ft damper open	150 ft damper closed	130 ft damper open	130 ft damper closed	100 ft damper open	100 ft damper closed	50 ft damper open	50 ft damper closed
minimum	17	16	1	2	24	19	44	27
5 th	26	22	2	3	42	23	48	35
50 th	88	45	5	7	98	53	121	57
mean	130	133	92	134	349	130	1101	58
95 th	368	351	694	875	1518	476	4454	85
maximum	810	3328	1092	1025	6717	1071	8880	215
sampling intervals (15-sec avg)	200	136	160	36	237	136	20	107
minutes	50.00	34.00	40.00	9.00	59.25	34.00	5.00	26.75
%	19	13	16	4	23	13	2	10

Table 4. Elapsed time, meteorological, monitoring, and operating condition factors for selected OWB sample periods.

	Figure 1	Figure 2
Elapsed time (min)	25	20
Sampling intervals (15-sec avg)	100	80
Relative humidity (%)	28	49-51
Temperature (°C)	5.8-3.5	6.5-6.1
Wind speed, direction	Calm/variable	calm/variable, light southerly
Precipitation	intermittent light snow	light snow
Monitoring instrument (DR) distance from OWB (ft)	130	100
OWB air intake mode	damper open	damper open/closed
Time from load, amount of fuel	~24 hr 1 wheelbarrow	during sample one-half wheelbarrow